

(A1.)

Thermo

$$V = V_0 + ap + bp^2$$

$$\text{where } a = -0.715 \times 10^{-3} \frac{\text{cm}^3}{\text{mole} \cdot \text{atm}}$$

$$b = 0.046 \times 10^{-6} \frac{\text{cm}^3}{\text{mole} \cdot \text{atm}^2}$$

$$dV = a dp + 2b p dp$$

$$\int_{P_1}^{P_2} p dV = \int_{P_1}^{P_2} p (a + 2bp) dp = a \frac{P_2^2 - P_1^2}{2} + \frac{2}{3} b (P_2^3 - P_1^3)$$

$$= -0.715 \times 10^{-3} \frac{1.01^2 (10^6 - 1)}{2} + \frac{2}{3} 0.046 \times 10^{-6} \cdot 1.01^3 (10^9 - 1) (\text{cm}^3 \cdot \text{atm})$$

$$= -0.333 \times 10^3 \text{ cm}^3 \cdot \text{atm} = -0.333 \times 10^3 \times 10^{-6} \times 1.01 \times 10^5 \text{ J} = -33.3 \text{ J}$$

This is work done by water

work by environment = +33.3 J

Thermo

(A4)

(a) The loss of the entropy in the hot reservoir is $\frac{Q}{T_h}$,

$$T_h = 500 \text{ K}$$

The gain of the entropy in the cold reservoir is $\frac{Q}{T_c}$, $T_c = 300 \text{ K}$

$$\Delta S = \frac{Q}{T_c} - \frac{Q}{T_h} = Q \left(\frac{1}{T_c} - \frac{1}{T_h} \right) = 500 \left(\frac{1}{300} - \frac{1}{500} \right) = 0.667 \frac{\text{J}}{\text{K}}$$

(b)

$$\text{Carnot efficiency} = 1 - \frac{T_c}{T_h}$$

$$W = Q \left(1 - \frac{T_c}{T_h} \right) = T_c \Delta S = 200 \text{ J}$$

(B1)

Thermo

$$\Delta Q = p \Delta V + c_v \Delta T$$

(a)

$$(i) \quad p = \text{const} \quad W = p \Delta V = p \left(\frac{RT_2}{p} - \frac{RT_1}{p} \right) = R \Delta T$$

$$\Delta U = \frac{5}{2} R \Delta T$$

$$\Delta Q = \frac{7}{2} R \Delta T$$

$$\frac{W}{\Delta Q} = \frac{2}{7}$$

$$(ii) \quad T = \text{const} \quad W = RT \ln \frac{V_2}{V_1}$$

$$\Delta U = 0 \quad \frac{W}{\Delta Q} = 1$$

(b) (ii) The process is reversible

$$\Delta S = \int \frac{dQ}{T} = \frac{1}{T} \int p dV = R \int_{V_1}^{V_2} \frac{1}{V} dV = R \ln \frac{V_2}{V_1}$$

(i) The process is irreversible, but we can make it

Quasistatic, so still

$$\Delta S = \int \frac{dQ}{T} = \int_{T_1}^{T_2} \frac{7}{2} R \frac{dT}{T} = \frac{7}{2} R \ln \frac{T_2}{T_1}$$

Thermos

B4.

The probability is given by binomial distribution

$$W(n_1, n_2) = \frac{N!}{n_1! n_2!} p^{n_1} q^{n_2} \quad N = n_1 + n_2$$

where n_1 the number of hops to the right
 n_2 to the left, and p, q are corresponding probabilities

~~from~~ position is given by $m = n_1 - n_2$

(a) $N=10, m=2 \quad n_1 = \frac{1}{2}(N+m) = 6, n_2 = 4, p=q = \frac{1}{2}$

$$W(6, 4) = \frac{10!}{6! 4!} \left(\frac{1}{2}\right)^{10} = \frac{10 \cdot 9 \cdot 8 \cdot 7}{6 \cdot 4 \cdot 2^{10}} = 0.205$$

$$m=4 \quad n_1 = 7, n_2 = 3$$

$$W(7, 3) = \frac{10!}{7! 3!} \left(\frac{1}{2}\right)^{10} = \frac{120}{2^{10}} = 0.117$$

(b) $\bar{n}_{\text{right}} = N \cdot p = 5 \quad \bar{n}_{\text{left}} = 5$

(c) $W(6, 4) = 210 \left(\frac{4}{5}\right)^6 \cdot \left(\frac{1}{5}\right)^4 = 0.088 \quad p = \frac{4}{5}, q = \frac{1}{5}$

$$W(7, 3) = 120 \left(\frac{4}{5}\right)^7 \left(\frac{1}{5}\right)^3 = 0.201$$

$$\bar{n}_{\text{right}} = Np = 8$$

$$\bar{n}_{\text{left}} = Nq = 2$$

A2. Solution:

For ideal gas, $V = nRT/P$.

$$\text{So, } \left(\frac{\partial V}{\partial T}\right)_P = \frac{nR}{P}, \left(\frac{\partial V}{\partial P}\right)_T = -\frac{nRT}{P^2}.$$

$$\alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_P = \frac{nR}{PV} = \frac{1}{T}, \quad K_T = -\frac{1}{V} \left(\frac{\partial V}{\partial P}\right)_T = -\frac{1}{V} \left(-\frac{nRT}{P^2}\right) = \frac{1}{P}.$$

A3. In a game, you repeatedly roll a standard die with the numbers 1 through 6 on its faces. If you roll a 6, the game is over. If you roll any other number, you may roll again.

- What is the probability that the game is still not over after N rolls?
- What is the probability that you roll a 6 in the N -th roll (so the game is over then)?
- What is the average number of rolls a player makes in this game? Hint: $(d/du)u^a = au^{a-1}$

Answers

Part a.

Probability to roll a 1, 2, 3, 4, or 5: $p = \frac{5}{6}$

Probability to roll a 6: $q = 1 - p = \frac{1}{6}$

Probability that game is still not over after N rolls is $\left(\frac{5}{6}\right)^N$

Part b.

Probability that game is not over after $N-1$ rolls is $\left(\frac{5}{6}\right)^{N-1}$

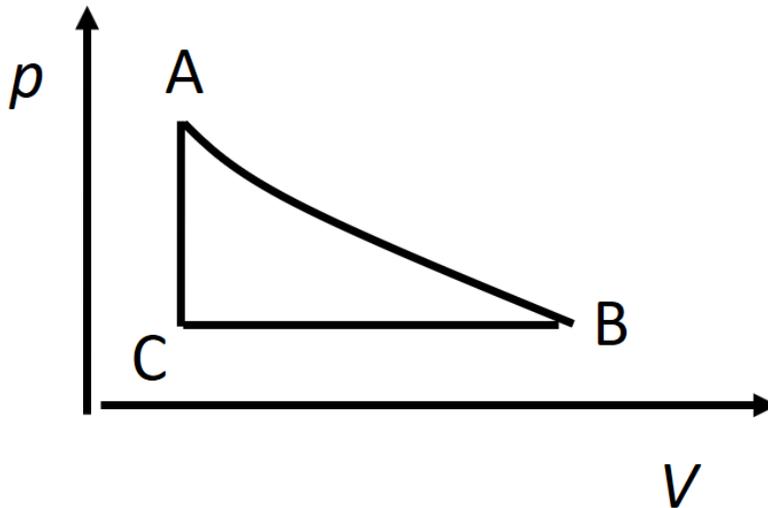
Probability for a 6 in the N -th role is $\frac{1}{6}$ (and then the game is over).

So the answer is $\left(\frac{5}{6}\right)^{N-1} \left(\frac{1}{6}\right)$

Part c.

$$\begin{aligned} \langle N \rangle &= \sum_{N=1}^{\infty} N p^{N-1} q = \sum_{N=1}^{\infty} N p^{N-1} (1-p) = (1-p) \sum_{N=1}^{\infty} \frac{d}{dp} p^N = (1-p) \frac{d}{dp} \sum_{N=1}^{\infty} p^N = \\ &= (1-p) \frac{d}{dp} \left(\frac{1}{1-p} \right) = (1-p) \frac{-1}{(1-p)^2} (-1) = \frac{1-p}{(1-p)^2} = \frac{1}{1-p} = \frac{1}{1-\frac{5}{6}} = 6 \end{aligned}$$

B2. Solution:



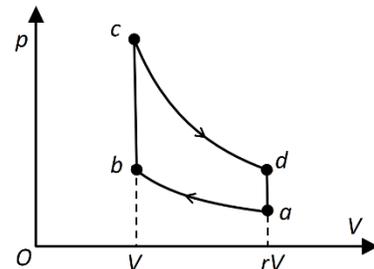
Assume the temperature of A and B is T ,
 $T_C = P_{BC} V_{AC} / R = \frac{1}{2} P_{BC} V_B / R = \frac{1}{2} T$.
 We then write everything in terms of T .

	ΔU	Q	W
A→B	0	$RT \ln(2)$	$RT \ln(2)$
B→C	$-3/4 RT$	$-5/4 RT$	$-RT/2$
C→A	$3/4 RT$	$3/4 RT$	0

The total work is $W = RT [\ln(2) - 1/2]$
 The total heat in is $Q = RT [\ln(2) + 3/4]$
 The efficiency is then $W/Q_{in} = 13.4\%$.

B3.

Consider a one-cylinder Otto-cycle engine with $r = 10.6$. The diameter of the cylinder is 82.5 mm. The distance that the piston moves during the compression is 86.4 mm. The initial pressure (at point a) of the gas/air mixture is 8.50×10^4 Pa, and the initial temperature is 300 K (the same as the outside air). Assume that 200 J of heat is added to the cylinder in each cycle by the burning gasoline, and that the gas has $C_v = 20.5$ J/(mol · K) and $\gamma = 1.40$.



- Calculate the volume of the air-fuel mixture at point a in the cycle.
- Calculate the amount of the mixture in moles.

- c. Calculate the temperature of the mixture at points b , c , and d in the cycle.
 d. Calculate the efficiency of this engine and compare it with the efficiency of a Carnot-cycle engine operating between the same maximum and minimum temperature.

Solution

(a) The change of the volume

$$\Delta V = A\Delta L = rV - V$$

where $A = \pi D^2/4$ is the area of the base of the cylinder

$$V_b = V = \frac{A\Delta L}{r-1} = \frac{\pi D^2\Delta L}{4(r-1)} = 4.81 \times 10^{-5} \text{m}^3.$$

$$V_a = rV = 5.10 \times 10^{-4} \text{m}^3.$$

(b)

$$p_a V_a = nRT_a, \quad n = \frac{p_a V_a}{RT_a} = \frac{8.5 \times 10^4 \cdot 5.10 \times 10^{-4}}{8.314 \cdot 300} = 0.01738 \text{ mole.}$$

(c) Point b: For the adiabatic process

$$T_a(rV)^{\gamma-1} = T_b V^{\gamma-1},$$

$$T_b = T_a r^{\gamma-1} = 771 \text{ K,}$$

Point c: Heat added

$$Q_H = nC_V(T_c - T_b),$$

therefore

$$T_c = \frac{Q_H}{nC_V} + T_b = \frac{200}{0.01738 \cdot 20.5} + 771 = 1332 \text{ K.}$$

Point d: For the adiabatic process, since $V_c = V$, $V_d = rV$,

$$T_d(rV)^{\gamma-1} = T_cV^{\gamma-1},$$

$$T_d = T_c/r^{\gamma-1} = 518 \text{ K.}$$

(d) The rejected heat in $d \rightarrow a$

$$|Q_C| = nC_V(T_d - T_a) = 78 \text{ J.}$$

The efficiency

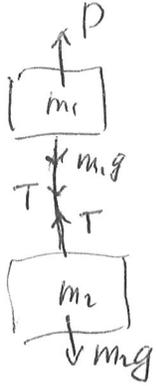
$$e = \frac{Q_H - |Q_C|}{Q_H} = 0.61$$

The Carnot efficiency

$$e_{Carnot} = 1 - \frac{T_C}{T_H} = 1 - 300/1332 = 0.775$$

is larger as should be.

A1.



$$P - T - m_1 g = m_1 a$$

$$P_1 = m_1 g \quad P_2 = m_2 g$$

$$T - m_2 g = m_2 a$$

add:

$$P - (m_1 + m_2)g = (m_1 + m_2)a$$

$$a = \frac{P - (m_1 + m_2)g}{m_1 + m_2} = g \frac{P - (P_1 + P_2)}{P_1 + P_2}$$

$$T = m_2(g + a) = m_2 \left(g + \frac{P - (m_1 + m_2)g}{m_1 + m_2} \right) = \frac{m_2 P}{m_1 + m_2}$$

$$(u) \quad \frac{T}{P} = \frac{m_2}{m_1 + m_2} = \frac{P_2}{P_1 + P_2} = 0.8$$

$$a = g \frac{150 - 125}{125} = 0.2g$$

A2.

The energy loss is $-mgh$
is equal to the energy loss due to Friction

$$-mgh = -\frac{\Delta E}{L} x \quad \text{where } x \text{ is the distance travelled}$$

$$x = L \frac{mgh}{\Delta E} = \frac{2.407}{0.688} L = 3.50L$$

So it traverses the flat region 3.5 times, therefore
it travels to the left when stops.

$$\mu \Delta E = FL = \mu mgL$$

$$\mu = \frac{\Delta E}{mgL} = \frac{0.688}{2.407} = 0.286$$

A3.

$$x(t) = A \cos \omega t$$

$$y(t) = -A \omega \sin \omega t$$

$$\text{for } t = t_1 \quad x(t_1) = \frac{1}{2} A = A \cos \omega t_1 \rightarrow \omega t_1 = \pm \frac{\pi}{3}$$

$$v(t_1) = 0.3 = -A \omega \sin \omega t_1$$

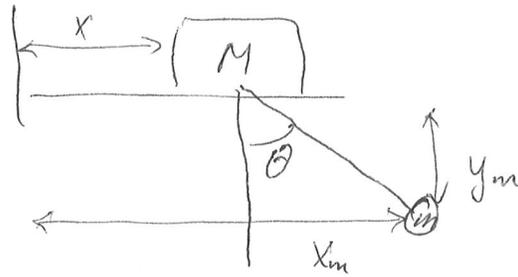
$$0.3 = \mp A \omega \sin \frac{\pi}{3} = \mp A \omega \frac{\sqrt{3}}{2}, \quad A = 0.1 \text{ m}$$

$$\omega = \frac{2}{\sqrt{3}} \frac{0.3}{0.1} = 2\sqrt{3} \text{ rad/s}$$

$$m = \frac{k}{\omega^2} = \frac{6 \text{ N/m}}{12 \text{ s}^{-2}} = 0.5 \text{ kg}$$

$$T = \frac{2\pi}{\omega} = \frac{\pi}{\sqrt{3}} \text{ s}$$

A4.



Coordinates of the bob:

$$\begin{aligned}x_m &= x + l \sin \theta & \text{therefore} & \quad \dot{x}_m = \dot{x} + l \dot{\theta} \cos \theta \\y_m &= -l \cos \theta & & \quad \dot{y}_m = l \dot{\theta} \sin \theta\end{aligned}$$

$$\begin{aligned}T &= \frac{1}{2} M \dot{x}^2 + \frac{1}{2} m [(\dot{x} + l \dot{\theta} \cos \theta)^2 + l^2 \dot{\theta}^2 \sin^2 \theta] \\&= \frac{1}{2} (M+m) \dot{x}^2 + \frac{1}{2} m l^2 \dot{\theta}^2 + m l \cos \theta \dot{\theta} \dot{x}\end{aligned}$$

$$U = -m g l \cos \theta$$

$$L = T - U$$

B1. (a) From Bernoulli's law

$$p_1 + \rho g y_1 + \frac{1}{2} \rho v_1^2 = p_3 + \rho g y_3 + \frac{1}{2} \rho v_3^2$$

$$p_1 = p_3 = p_{atm}, v_1 = 0, \text{ therefore}$$

$$v_3^2 = 2g(y_1 - y_3) = 2 \cdot 9.8 \cdot 8$$

$$v_3 = 12.5 \frac{m}{s}$$

$$A_3 v_3 = A_2 v_2 \quad 0.048 \cdot v_2 = 0.016 \cdot 12.5$$

$$v_2 = \frac{12.5}{3} = 4.17 \frac{m}{s}$$

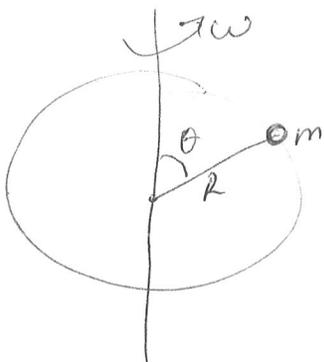
$$(b) \text{ rate} = A_3 v_3 = 0.016 \cdot 12.5 = 0.2 \frac{m^3}{s}$$

$$(c) \quad p_2 + \frac{1}{2} \rho v_2^2 = p_3 + \frac{1}{2} \rho v_3^2$$

$$p_2 = p_3 + \frac{1}{2} \rho (v_3^2 - v_2^2) = 1.013 \times 10^5 + \frac{1}{2} \times 10^3 \frac{kg}{m^3} (156.25 - 17.36)$$

$$= 17.07 \times 10^4 Pa$$

B2



$$(a) \quad T = \frac{1}{2} m R^2 \dot{\theta}^2 + \frac{1}{2} m (R \sin \theta)^2 \omega^2$$

$$U = mg R \cos \theta$$

$$L = T - U = \frac{1}{2} m R^2 (\dot{\theta}^2 + \omega^2 \sin^2 \theta) - mg R \cos \theta$$

$$\frac{\partial L}{\partial \theta} = m R^2 \omega^2 \sin \theta \cos \theta + mg R \sin \theta$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\theta}} \right) = \frac{d}{dt} (m R^2 \dot{\theta}) = m R^2 \ddot{\theta}$$

$$\ddot{\theta} - \omega^2 \sin \theta \cos \theta - \frac{g}{R} \sin \theta = 0$$

(b) equilibrium: $\ddot{\theta} = 0$

$$-\omega^2 \sin \theta \cos \theta - \frac{g}{R} \sin \theta = 0$$

$$\theta_1 = 0, \theta_2 = \pi, \theta_3 = \cos^{-1} \left(-\frac{g}{R \omega^2} \right)$$

(c) expand the function

$$f(\theta) = -\omega^2 \sin \theta \cos \theta - \frac{g}{R} \sin \theta \quad \text{near the equilibrium}$$

$$f(\theta) = f(\theta_i) - \left[\omega^2 \cos 2\theta_i + \frac{g}{R} \cos \theta_i \right] (\theta - \theta_i) \quad i=1, 2, 3, f(\theta_i) = 0$$

for stable equilibrium we need

$$-\omega^2 \cos 2\theta_i - \frac{g}{R} \cos \theta_i > 0$$

$i=1$: $-\omega^2 - \frac{g}{R} > 0$ impossible, therefore equilibrium is always unstable

(B2), p. 2

$$i=2 \quad -\omega^2 + \frac{g}{R} > 0$$

Stable for $\omega^2 < \frac{g}{R}$

$$i=3 \quad \cos \theta_3 = -\frac{g}{R\omega^2} \quad \cos 2\theta_3 = 2\cos^2 \theta_3 - 1 = 2\left(\frac{g}{R\omega^2}\right)^2 - 1$$

$$-\omega^2 \left[2\left(\frac{g}{R\omega^2}\right)^2 - 1 \right] + \frac{g}{R} \frac{g}{R\omega^2} > 0$$

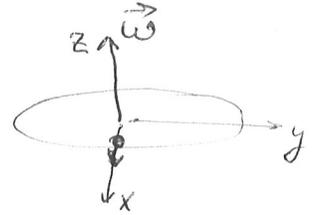
$$-\left(\frac{g}{R\omega}\right)^2 + \omega^2 > 0 \quad \omega^4 > \left(\frac{g}{R}\right)^2$$

Stable for $\omega^2 > \frac{g}{R}$

B3.

The effective force is opposite to ~~for~~ the sum of inertial forces in the rotating frame:

Centrifugal $\vec{F}_{cf} = -m\vec{\omega} \times (\vec{\omega} \times \vec{r})$
 Coriolis $\vec{F}_{cor} = -2m\vec{\omega} \times \dot{\vec{r}}$
 Transverse force $\vec{F}_{trans} = -m\dot{\vec{\omega}} \times \vec{r}$



$$\vec{F}_{~~net~~} = -m\vec{\omega} \times (\vec{\omega} \times \vec{r}) - 2m\vec{\omega} \times \dot{\vec{r}} - m\dot{\vec{\omega}} \times \vec{r}$$

$$\dot{\vec{\omega}} = 0 \quad \vec{\omega} \times \vec{r} = \omega r \hat{z} \times \hat{x} = \omega r \hat{y}$$

$$\vec{\omega} \times (\vec{\omega} \times \vec{r}) = \omega^2 r (\hat{z} \times \hat{y}) = -\omega^2 r \hat{x}$$

$$\vec{F}_{cf} = \omega^2 r \hat{x}$$

$$\vec{F}_{cor} = -2m\vec{\omega} \times \dot{\vec{r}} = -2m\omega v \hat{z} \times \hat{x} = -2m\omega v \hat{y}$$

$$\vec{F}_{~~net~~} = m\omega^2 r \hat{x} - 2m\omega v \hat{y}$$

The effective force in the inertial frame $\vec{F}_{eff} = -\vec{F}_{~~net~~}$

(b)

Balance friction with $\vec{F}_{~~net~~}$

$$\mu mg = \left[(m\omega^2 r)^2 + (2m\omega v)^2 \right]^{1/2}$$

$$(\mu g)^2 = (\omega^2 r)^2 + (2\omega v)^2$$

$$r = \frac{[(\mu g)^2 - (2\omega v)^2]^{1/2}}{\omega}$$

This is the maximum possible value of r before the ant starts to slip

B4

Conservation of energy

$$mgh = \frac{mv^2}{2} + \frac{I\omega^2}{2} = \frac{mv^2}{2} + \frac{Iv^2}{2R^2}$$

$$m\left(gh - \frac{v^2}{2}\right) = \frac{Iv^2}{2R^2}$$

$$I = \frac{2mR^2}{v^2} \left(gh - \frac{v^2}{2}\right) = mR^2 \left(\frac{2gh}{v^2} - 1\right)$$

Find v from kinematics
For constant acceleration

$$h = \frac{at^2}{2} = \frac{v}{2}t \quad \text{since } a = \frac{v}{t}$$

$$v = \frac{2h}{t}$$

$$\begin{aligned} \text{(a)} \quad I &= mR^2 \left(\frac{gt^2}{2h} - 1\right) = 8.2 \cdot 0.35^2 \cdot \left(\frac{9.8 \cdot 16}{2 \cdot 12} - 1\right) \\ &= 5.56 \text{ kg} \cdot \text{m}^2 \end{aligned}$$

$$\text{(b)} \quad a = \frac{2h}{t^2} = \frac{24}{16} = 1.5 \frac{\text{m}}{\text{s}^2}$$

$$\text{(c)} \quad \alpha = \frac{a}{R} = \frac{1.5}{0.35 \text{ m}} = 4.29 \frac{\text{rad}}{\text{s}^2}$$